



3.1V<sub>IN</sub> to 31V<sub>IN</sub> Isolated µModule DC/DC Converter

- 2kV AC Isolated µModule Converter (Tested at 3kVDC)
- $\blacksquare$  UL60950 Recognized File 464570  $\epsilon$  $\mathbf{N}_{\text{us}}$
- Wide Input Voltage Range: 3.1V to 31V
- **u** Up to 440mA Output Current ( $V_{IN} = 24V$ ,  $V_{OUT1} = 2.5V$ ) **Output Adjustable from 2.5V to 12V**
- Current Mode Control
- Programmable Soft-Start
- User Configurable Undervoltage Lockout
- Ullet Low Profile (9mm  $\times$  11.25mm  $\times$  4.92mm) BGA Package

## **APPLICATIONS**

- Industrial Sensors
- $\blacksquare$  Industrial Switches
- Test and Measurement Equipment

## TYPICAL APPLICATION



## FEATURES DESCRIPTION

The LTM<sup>®</sup>8057 is a 2kV AC isolated flyback µModule<sup>®</sup> (micromodule) DC/DC converter. Included in the package are the switching controller, power switches, transformer, and all support components. Operating over an input voltage range of 3.1V to 31V, the LTM8057 supports an output voltage range of 2.5V to 12V, set by a single resistor. Only output and input capacitors are needed to finish the design. Other components may be used to control the soft-start control and biasing.

The LTM8057 is packaged in a thermally enhanced, compact (9mm  $\times$  11.25mm  $\times$  4.92mm) overmolded ball grid array (BGA) package suitable for automated assembly by standard surface mount equipment. The LTM8057 is available with SnPb or RoHS compliant terminal finish.

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#### **Maximum Output Current vs VIN 2kV AC Isolated µModule Regulator**



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## ABSOLUTE MAXIMUM RATINGS PIN CONFIGURATION

**(Note 1)**





#### ORDER INFORMATION **http://www.linear.com/product/LTM8057#orderinfo**



Consult Marketing for parts specified with wider operating temperature ranges. \*Device temperature grade is indicated by a label on the shipping container. Pad or ball finish code is per IPC/JEDEC J-STD-609.

• Terminal Finish Part Marking: www.linear.com/leadfree

• Recommended LGA and BGA PCB Assembly and Manufacturing Procedures:

www.linear.com/umodule/pcbassembly

• LGA and BGA Package and Tray Drawings: www.linear.com/packaging

## ELECTRICAL CHARACTERISTICS The  $\bullet$  denotes the specifications which apply over the full internal

operating temperature range, otherwise specifications are at  $T_A$  = 25°C, RUN = 12V (Note 4).



**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:**  $V_{IN}$  +  $V_{OUT}$  is defined as the sum of  $(V_{IN} - GND)$  +  $(V_{OUT} - V_{OUT}$ . **Note 3:** The LTM8057 isolation is tested at 3kV DC for one second.

**Note 4:** The LTM8057E is guaranteed to meet performance specifications from 0°C to 125°C. Specifications over the –40°C to 125°C internal temperature range are assured by design, characterization and correlation with statistical process controls. LTM8057I is guaranteed to meet

specifications over the full -40°C to 125°C internal operating temperature range. The LTM8057MP is guaranteed to meet specifications over the full –55°C to 125°C internal operating temperature range. Note that the maximum internal temperature is determined by specific operating conditions in conjunction with board layout, the rated package thermal resistance and other environmental factors.

Test flowcharts are posted for viewing at:

www.linear.com/quality

**Note 5:** This is the BIAS pin voltage at which the internal circuitry is powered through the BIAS pin and not the integrated regulator. See BIAS Pin Considerations for details.

# TYPICAL PERFORMANCE CHARACTERISTICS **Unless otherwise noted, operating conditions are**

as in Table 1 ( $T_A = 25^\circ \text{C}$ ).

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## TYPICAL PERFORMANCE CHARACTERISTICS **Unless otherwise noted, operating conditions are**

**as in Table 1 (TA = 25°C).**



8057 G16

8057 G15

## TYPICAL PERFORMANCE CHARACTERISTICS **Unless otherwise noted, operating conditions are**

as in Table 1 ( $T_A = 25^{\circ}C$ ).





**Minimum Required Load vs Input Voltage**



**Typical Output Ripple 100mA Output Current, V<sub>IN</sub> = 12V** 



MEASURED ON DC1987 WITH ADDIONAL 1µF AND BNC ATTACHED TO OUTPUT TERMINALS. C7 = 0.1µF. USED HP461A 150MHz AMPLIFIER, SET TO 40dB GAIN.

**DC1988 VOUT1 Start-Up Behavior**  for Different C<sub>SS</sub> Values



**Typical Switching Frequency vs Output Current Stock DC1988A**



8057 G22



**Junction Temperature Rise vs Load Current**



www.datasheetall.com

## TYPICAL PERFORMANCE CHARACTERISTICS **Unless otherwise noted, operating conditions are**

**as in Table 1 (TA = 25°C).**







**Junction Temperature Rise vs Load Current** 10  $V<sub>OUT</sub> = 5V$ 9 وبالمحا 8 TEMPERATURE RISE (°C) TEMPERATURE RISE (°C) 7 6 5 4 3  $3.3V_{\text{IN}}$ 2  $-5V_{IN}$  $12V_{IN}$ 1  $- - - 24V_{IN}$ 0 0 100 50 150 200 300250 350 V<sub>OUT</sub> LOAD CURRENT (mA) 8057 G26

**Junction Temperature Rise vs Load Current**



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## PIN FUNCTIONS



#### **PACKAGE ROW AND COLUMN LABELING MAY VARY AMONG µModule PRODUCTS. REVIEW EACH PACKAGE LAYOUT CAREFULLY.**

 $V_{\text{OUT}}$  (Bank 1):  $V_{\text{OUT}}$  and  $V_{\text{OUT}}$  comprise the isolated output of the LTM8057 flyback stage. Apply an external capacitor between  $V_{\text{OUT}}$  and  $V_{\text{OUT}}^-$ . Do not allow  $V_{\text{OUT}}^-$  to  $exceed$   $V<sub>OIII</sub>$ .

 $V_{\text{OUT}}$ <sup>-</sup> (Bank 2):  $V_{\text{OUT}}$ <sup>-</sup> is the return for both  $V_{\text{OUT1}}$  and  $V<sub>OUT2</sub>$ .  $V<sub>OUT1</sub>$  and  $V<sub>OUT</sub>$  comprise the isolated output of the LTM8057. In most applications, the bulk of the heat flow out of the LTM8057 is through the GND and  $V_{OUT}^$ pads, so the printed circuit design has a large impact on the thermal performance of the part. See the PCB Layout and Thermal Considerations sections for more details. Apply an external capacitor between  $V_{\text{OUT}}$  and  $V_{\text{OUT}}$ .

**GND (Bank 4):** This is the primary side local ground of the LTM8057 primary. In most applications, the bulk of the heat flow out of the LTM8057 is through the GND and  $V_{OUT}$ pads, so the printed circuit design has a large impact on the thermal performance of the part. See the PCB Layout and Thermal Considerations sections for more details.

 $V_{IN}$  (Bank 5):  $V_{IN}$  supplies current to the LTM8057's internal regulator and to the integrated power switch. These pins must be locally bypassed with an external, low ESR capacitor.

**RUN (Pin F3):** A resistive divider connected to  $V_{IN}$  and this pin programs the minimum voltage at which the LTM8057 will operate. Below 1.24V, the LTM8057 does not deliver power to the secondary. Above 1.24V, power will be delivered to the secondary and 10µA will be fed into the SS pin. When RUN is less than 1.24V, the pin draws 2.5µA, allowing for a programmable hysteresis. Do not allow a negative voltage (relative to GND) on this pin. Tie this pin to  $V_{IN}$  if it is not used.

**ADJ (Pins G7):** Apply a resistor from this pin to GND to set the output voltage  $V_{\text{OUT}}$  relative to  $V_{\text{OUT}}$ , using the recommended value given in Table 1. If Table 1 does not list the desired  $V_{\text{OUT}}$  value, the equation:

$$
R_{ADJ} = 28.4 (V_{OUT1}^{-0.879}) k\Omega
$$

may be used to approximate the value. To the seasoned designer, this exponential equation may seem unusual. The equation is exponential due to nonlinear current sources that are used to temperature compensate the regulation.

**BIAS (Pin H5):** This pin supplies the power necessary to operate the LTM8057. It must be locally bypassed with a low ESR capacitor of at least 4.7μF. Do not allow this pin voltage to rise above V<sub>IN</sub>.

**SS (Pin H6):** Place a soft-start capacitor here to limit inrush current and the output voltage ramp rate. Do not allow a negative voltage (relative to GND) on this pin.

## BLOCK DIAGRAM



# **OPERATION**

The LTM8057 is a stand-alone isolated flyback switching DC/DC power supply that can deliver up to 440mA of output current. This module provides a regulated output voltage programmable via one external resistor from 2.5V to 12V. The input voltage range of the LTM8057 is 3.1V to 31V. Given that the LTM8057 is a flyback converter, the output current depends upon the input and output voltages, so make sure that the input voltage is high enough to support the desired output voltage and load current. The Typical Performance Characteristics section gives several graphs of the maximum load versus  $V_{IN}$  for several output voltages.

A simplified block diagram is given. The LTM8057 contains a current mode controller, power switching element, power transformer, power Schottky diode and a modest amount of input and output capacitance.

The LTM8057 has a galvanic primary to secondary isolation rating of 2kV AC. This is verified by applying 3kV DC between the primary and secondary for 1 second. Note that the 2kV AC isolation is verified by a 3kV DC test. The peak voltage of a 2kV AC waveform is 2.83kV DC, so 3kV DC is applied. For details please refer to the Isolation, Working Voltage and Safely Compliance section. The LTM8057 is a UL 60950 recognized component.

An internal regulator provides power to the control circuitry. The bias regulator normally draws power from the  $V_{IN}$  pin, but if the BIAS pin is connected to an external voltage higher than 3.1V, bias power will be drawn from the external source, improving efficiency.  $V_{BIAS}$  must not exceed  $V_{IN}$ . The RUN pin is used to turn on or off the LTM8057, disconnecting the output and reducing the input current to 1μA or less.

The LTM8057 is a variable frequency device. For a fixed input and output voltage, the frequency increases as the load increases. For light loads, the current through the internal transformer may be discontinuous.

For most applications, the design process is straight forward, summarized as follows:

- 1. Look at Table 1a and find the row that has the desired input range and output voltage.
- 2. Apply the recommended  $C_{IN}$ ,  $C_{OUT}$  and  $R_{AD,I}$  if required.
- 3. Connect BIAS as indicated, or tie to an external source up to 15V or  $V_{IN}$ , whichever is less.

While these component combinations have been tested for proper operation, it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental conditions. Bear in mind that the maximum output current may be limited by junction temperature, the relationship between the input and output voltage magnitude and polarity and other factors. Please refer to the graphs in the Typical Performance Characteristics section for guidance.

## **Capacitor Selection Considerations**

The C<sub>IN</sub> and C<sub>OUT</sub> capacitor values in Table 1 are the minimum recommended values for the associated operating conditions. Applying capacitor values below those indicated in Table 1 is not recommended, and may result in undesirable operation. Using larger values is generally acceptable, and can yield improved dynamic response, if it is necessary. Again, it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental conditions.

Ceramic capacitors are small, robust and have very low ESR. However, not all ceramic capacitors are suitable. X5R and X7R types are stable over temperature and applied voltage and give dependable service. Other types, including Y5V and Z5U have very large temperature and voltage coefficients of capacitance. In an application circuit they may have only a small fraction of their nominal capacitance resulting in much higher output voltage ripple than expected.

A final precaution regarding ceramic capacitors concerns the maximum input voltage rating of the LTM8057. A ceramic input capacitor combined with trace or cable inductance forms a high-Q (underdamped) tank circuit. If the LTM8057 circuit is plugged into a live supply, the input voltage can ring to much higher than its nominal value, possibly exceeding the device's rating. This situation is easily avoided; see the Hot-Plugging Safely section.

			.	$\cdots$	
V <sub>IN</sub>	V <sub>OUT</sub>	V <sub>BIAS</sub>	$c_{\rm IN}$	$c_{\text{out}}$	$R_{ADJ}$
3.1V to 31V	2.5V	3.1V to 15V or Open	2.2µF, 50V, 1206	100µF, 6.3V, 1210	12.4k
3.1V to 31V	3.3V	3.1V to 15V or Open	2.2µF, 50V, 1206	100µF, 6.3V, 1210	10k
3.1V to 29V	5V	3.1V to 15V or Open	2.2µF, 50V, 1206	22µF, 16V, 1210	6.98k
3.1V to 26V	8V	3.1V to 15V or Open	2.2µF, 50V, 1206	22µF, 10V, 1206	4.53k
3.1V to 24V	12V	3.1V to 15V or Open	2.2µF, 25V, 0805	10µF, 16V, 1210	3.16k/8.2pF*
9V to 15V	2.5V	$V_{\text{IN}}$	2.2µF, 50V, 1206	100µF, 6.3V, 1210	12.4k
9V to 15V	3.3V	$V_{IN}$	2.2µF, 50V, 1206	47µF, 6.3V, 1210	10k
9V to 15V	5V	$V_{IN}$	2.2µF, 50V, 1206	22µF, 16V, 1210	6.98k
9V to 15V	8V	$V_{IN}$	2.2µF, 50V, 1206	22µF, 10V, 1206	4.53k
9V to 15V	12V	$V_{\text{IN}}$	2.2µF, 25V, 0805	10µF, 16V, 1210	3.16k
18V to 31V	2.5V	3.1V to 15V or Open	2.2µF, 50V, 1206	100µF, 6.3V, 1210	12.4k
18V to 31V	3.3V	3.1V to 15V or Open	2.2µF, 50V, 1206	47µF, 6.3V, 1210	10k
18V to 29V	5V	3.1V to 15V or Open	2.2µF, 50V, 1206	22µF, 16V, 1210	6.98k
18V to 26V	8V	3.1V to 15V or Open	2.2µF, 50V, 1206	22µF, 10V, 1206	4.53k
18V to 24V	<b>12V</b>	3.1V to 15V or Open	2.2µF, 50V, 1206	10µF, 16V, 1210	3.16k/8.2pF*

**LTM8057 Table 1a. Recommended Component Values and Configuration for Specific V<sub>OUT</sub> Voltages (T<sub>A</sub> = 25°C)** 

Note: Do not allow BIAS to exceed V<sub>IN</sub>, a bulk input capacitor is required. If BIAS is open, the minimum V<sub>IN</sub> is 4.3V. \*Connect 3.16k in parallel with 8.2pF from ADJ to GND

## **BIAS Pin Considerations**

The BIAS pin is the output of an internal linear regulator that powers the LTM8057's internal circuitry. It is set to 3V and must be decoupled with a low ESR capacitor of at least 4.7μF. The LTM8057 will run properly without applying a voltage to this pin, but will operate more efficiently and dissipate less power if a voltage between 3.1V and  $V_{IN}$  is applied. At low  $V_{IN}$ , the LTM8057 will be able to deliver more output current if BIAS is 3.1V or greater. Up to 31V may be applied to this pin, but a high BIAS voltage will cause excessive power dissipation in the internal circuitry. For applications with an input voltage less than 15V, the BIAS pin is typically connected directly to the V<sub>IN</sub> pin. For input voltages greater than 15V, it is preferred to leave the BIAS pin separate from the  $V_{\text{IN}}$  pin, either powered from a separate voltage source or left running from the internal regulator. This has the added advantage of keeping the physical size of the BIAS capacitor small. Do not allow BIAS to rise above V<sub>IN</sub>.

## **Soft-Start**

For many applications, it is necessary to minimize the inrush current at start-up. The built-in soft-start circuit significantly reduces the start-up current spike and output voltage overshoot by applying a capacitor from SS to GND. When the LTM8057 is enabled, whether from  $V_{IN}$  reaching a sufficiently high voltage or RUN being pulled high, the LTM8057 will source approximately 10µA out of the SS pin. As this current gradually charges the capacitor from SS to GND, the LTM8057 will correspondingly increase the power delivered to the output, allowing for a graceful turn-on ramp.

## **Isolation, Working Voltage and Safety Compliance**

The LTM8057 isolation is 100% hi-pot tested by tying all of the primary pins together, all of the secondary pins together and subjecting the two resultant circuits to a differential of 3kV DC for one second. This establishes the isolation voltage rating of the LTM8057 component.

The isolation rating of the LTM8057 is not the same as the working or operational voltage that the application will experience. This is subject to the application's power source, operating conditions, the industry where the end product is used and other factors that dictate design requirements such as the gap between copper planes, traces and component pins on the printed circuit board, as well as the type of connector that may be used. To maximize the allowable working voltage, the LTM8057 has two columns of solder balls removed to facilitate the printed circuit board design. The ball to ball pitch is 1.27mm, and the typical ball diameter is 0.78mm. Accounting for the missing columns and the ball diameter, the printed circuit board may be designed for a metal-to-metal separation of up to 3.03mm. This may have to be reduced somewhat to allow for tolerances in solder mask or other printed circuit board design rules. For those situations where information about the spacing of LTM8057 internal circuitry is required, the minimum metal to metal separation of the primary and secondary is 0.75mm.

To reiterate, the manufacturer's isolation voltage rating and the required working or operational voltage are often different numbers. In the case of the LTM8057, the isolation voltage rating is established by 100% hi-pot testing. The working or operational voltage is a function of the end product and its system level specifications. The actual required operational voltage is often smaller than the manufacturer's isolation rating.

The LTM8057 is a UL recognized component under UL 60950, file number 464570. The UL 60950 insulation category of the LTM8057 transformer is Functional. Considering UL 60950 Table 2N and the gap distances stated above, 3.03mm external and 0.75mm internal, the LTM8057 may be operated with up to 250V working voltage in a pollution degree 2 environment. The actual working voltage, insulation category, pollution degree and other critical parameters for the specific end application depend upon the actual environmental, application and safety compliance requirements. It is therefore up to the user to perform a safety and compliance review to ensure that the LTM8057 is suitable for the intended application.

## **ADJ and Line Regulation**

For  $V_{\text{OUT}}$  greater than 8V, parasitics in the transformer interacting with the controller cause a localized increase in minimum load. A small capacitor may need to be applied from ADJ to GND to ensure proper line regulation. Care must be taken when choosing this capacitor value. Too small or no capacitor will result in poor line regulation; in general, a larger capacitor is needed for higher  $V_{OIII}$ . Too large of a capacitance will require excessive minimum load to maintain regulation.

The plots in Figure 1 show LTM8057 line regulation at three different capacitor values applied from ADJ to GND.

The plots in Figure 2 show the minimum load requirement for the same three capacitors.

Carefully choose the appropriate capacitor value for the intended application.



**Figure 1. V<sub>OUT</sub> Line Regulation vs V<sub>IN</sub>** 



**Figure 2. Minimum Required Load vs Input Voltage**

## V<sub>OUT</sub> to V<sub>OUT</sub> Reverse Voltage

The LTM8057 cannot tolerate a reverse voltage from  $V_{OUT}$ to  $V_{\text{OUT}}$  during operation. If  $V_{\text{OUT}}$  raises above  $V_{\text{OUT}}$  during operation, the LTM8057 may be damaged. To protect against this condition, a low forward drop power Schottky diode has been integrated into the LTM8057, anti-parallel to  $V_{\text{OUT}}/V_{\text{OUT}}$ . This can protect the output against many reverse voltage faults. Reverse voltage faults can be both steady state and transient. An example of a steady-state voltage reversal is accidentally misconnecting a powered LTM8057 to a negative voltage source. An example of transient voltage reversals is a momentary connection to a negative voltage. It is also possible to achieve a  $V_{\text{OIII}}$ reversal if the load is short circuited through a long cable. The inductance of the long cable forms an LC tank circuit with the  $V_{\text{OUT}}$  capacitance, which drive  $V_{\text{OUT}}$  negative. Avoid these conditions.

## **Safety Rated Capacitors**

Some applications require safety rated capacitors, which are high voltage capacitors that are specifically designed and rated for AC operation and high voltage surges. These capacitors are often certified to safety standards such as UL 60950, IEC 60950 and others. In the case of the LTM8057, a common application of a safety rated capacitor would be to connect it from GND to  $V_{OUT}$ . To provide maximum flexibility, the LTM8057 does not include any components between GND and  $V_{\text{OUT}}$ . Any safety capacitors must be added externally.

The specific capacitor and circuit configuration for any application depends upon the safety requirements of the system into which the LTM8057 is being designed. Table 2 provides a list of possible capacitors and their manufacturers. The application of a capacitor from GND to  $V_{\text{OUT}}$  may also reduce the high frequency output noise on the output.

#### **Table 2. Safety Rated Capacitors**



#### **PCB Layout**

Most of the headaches associated with PCB layout have been alleviated or even eliminated by the high level of integration of the LTM8057. The LTM8057 is nevertheless a switching power supply, and care must be taken to minimize electrical noise to ensure proper operation. Even with the high level of integration, you may fail to achieve specified operation with a haphazard or poor layout. See Figure 3 for a suggested layout. Ensure that the grounding and heat sinking are acceptable.

A few rules to keep in mind are:

- 1. Place the  $R_{ADJ}$  resistor as close as possible to their respective pins.
- 2. Place the C<sub>IN</sub> capacitor as close as possible to the V<sub>IN</sub> and GND connections of the LTM8057.
- 3. Place the C<sub>OUT1</sub> capacitor as close as possible to V<sub>OUT</sub> and  $V_{OIII}$ .
- 4. Place the C<sub>IN</sub> and C<sub>OUT</sub> capacitors such that their ground current flow directly adjacent or underneath the LTM8057.
- 5. Connect all of the GND connections to as large a copper pour or plane area as possible on the top layer. Avoid breaking the ground connection between the external components and the LTM8057.



**Figure 3. Layout Showing Suggested External Components, Planes and Thermal Vias**

6. Use vias to connect the GND copper area to the board's internal ground planes. Liberally distribute these GND vias to provide both a good ground connection and thermal path to the internal planes of the printed circuit board. Pay attention to the location and density of the thermal vias in Figure 3. The LTM8057 can benefit from the heat sinking afforded by vias that connect to internal GND planes at these locations, due to their proximity to internal power handling components. The optimum number of thermal vias depends upon the printed circuit board design. For example, a board might use very small via holes. It should employ more thermal vias than a board that uses larger holes.

## **Hot-Plugging Safely**

The small size, robustness and low impedance of ceramic capacitors make them an attractive option for the input bypass capacitor of the LTM8057. However, these capacitors can cause problems if the LTM8057 is plugged into a live supply (see Linear Technology Application Note 88 for a complete discussion). The low loss ceramic capacitor combined with stray inductance in series with the power source forms an underdamped tank circuit, and the voltage at the  $V_{\text{IN}}$  pin of the LTM8057 can ring to more than twice the nominal input voltage, possibly exceeding the LTM8057's rating and damaging the part. If the input supply is poorly controlled or the user will be plugging the LTM8057 into an energized supply, the input network should be designed to prevent this overshoot. This can be accomplished by installing a small resistor in series to  $V_{IN}$ , but the most popular method of controlling input voltage overshoot is adding an electrolytic bulk capacitor to the  $V_{IN}$  net. This capacitor's relatively high equivalent series resistance damps the circuit and eliminates the voltage overshoot. The extra capacitor improves low frequency ripple filtering and can slightly improve the efficiency of the circuit, though it can be a large component in the circuit.

## **Thermal Considerations**

The LTM8057 output current may need to be derated if it is required to operate in a high ambient temperature. The amount of current derating is dependent upon the input voltage, output power and ambient temperature. The temperature rise curves given in the Typical Performance Characteristics section can be used as a guide. These curves were generated by the LTM8057 mounted to a 58cm<sup>2</sup> 4-layer FR4 printed circuit board. Boards of other sizes and layer count can exhibit different thermal behavior, so it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental operating conditions.

For increased accuracy and fidelity to the actual application, many designers use FEA to predict thermal performance. To that end, the Pin Configuration section of the data sheet typically gives four thermal coefficients:

 $\theta_{JA}$ : Thermal resistance from junction to ambient

θJCbottom: Thermal resistance from junction to the bottom of the product case

θJCtop: Thermal resistance from junction to top of the product case

θJCboard: Thermal resistance from junction to the printed circuit board.

While the meaning of each of these coefficients may seem to be intuitive, JEDEC has defined each to avoid confusion and inconsistency. These definitions are given in JESD 51-12, and are quoted or paraphrased as follows:

θJA is the natural convection junction-to-ambient air thermal resistance measured in a one cubic foot sealed enclosure. This environment is sometimes referred to as still air although natural convection causes the air to move. This value is determined with the part mounted to a JESD 51-9 defined test board, which does not reflect an actual application or viable operating condition.

 $\theta$ JC<sub>hottom</sub> is the junction-to-board thermal resistance with all of the component power dissipation flowing through the bottom of the package. In the typical µModule converter, the bulk of the heat flows out the bottom of the package, but there is always heat flow out into the ambient environment. As a result, this thermal resistance value may be useful for comparing packages but the test conditions don't generally match the user's application.

 $\theta$ <sub>JCtop</sub> is determined with nearly all of the component power dissipation flowing through the top of the package. As the electrical connections of the typical µModule converter are on the bottom of the package, it is rare for an application to operate such that most of the heat flows from the junction to the top of the part. As in the case of  $\theta_{JChottom}$ , this value may be useful for comparing packages but the test conditions don't generally match the user's application.

 $\theta_{\text{JCboard}}$  is the junction-to-board thermal resistance where almost all of the heat flows through the bottom of the µModule converter and into the board, and is really the sum of the θJCbottom and the thermal resistance of the bottom of the part through the solder joints and through a portion of the board. The board temperature is measured a specified distance from the package, using a two-sided, two-layer board. This board is described in JESD 51-9.

Given these definitions, it should now be apparent that none of these thermal coefficients reflects an actual physical operating condition of a µModule converter. Thus, none of them can be individually used to accurately predict the thermal performance of the product. Likewise, it would be inappropriate to attempt to use any one coefficient to correlate to the junction temperature vs load graphs given in the product's data sheet. The only appropriate way to use the coefficients is when running a detailed thermal analysis, such as FEA, which considers all of the thermal resistances simultaneously.

A graphical representation of these thermal resistances is given in Figure 4.

The blue resistances are contained within the  $µ$ Module converter, and the green are outside.

The die temperature of the LTM8057 must be lower than the maximum rating of 125°C, so care should be taken in the layout of the circuit to ensure good heat sinking of the LTM8057. The bulk of the heat flow out of the LTM8057 is through the bottom of the module and the BGA pads into the printed circuit board. Consequently a poor printed circuit board design can cause excessive heating, resulting in impaired performance or reliability. Please refer to the PCB Layout section for printed circuit board design suggestions.





### **3.3V Flyback Converter Maximum Output Current vs V<sub>IN</sub>**



**2.5V Flyback Converter**



#### **8V Flyback Converter**



**Maximum Output Current vs VIN** 



**Maximum Output Current vs V<sub>IN</sub>** 



## PACKAGE DESCRIPTION



#### **Pin Assignment Table (Arranged by Pin Number)**

## PACKAGE PHOTO



## PACKAGE DESCRIPTION

**Please refer to http://www.linear.com/product/LTM8057#packaging for the most recent package drawings.**



tion that the interconnection of its circuits as described herein will not infringe on existing patent rights. Information furnished by Linear Technology Corporation is believed to be accurate and reliable. However, no responsibility is assumed for its use. Linear Technology Corporation makes no representa-

## REVISION HISTORY



## TYPICAL APPLICATION

**12V Flyback Converter with Low Noise Bypass <b>Maximum Output Current vs V<sub>IN</sub>** 



## DESIGN RESOURCES



## RELATED PARTS









 $V_{IN}$  (V)

20

8057 TA05b