



LTM8026

- Complete Step-Down Switch Mode Power Supply
- Constant-Voltage Constant-Current Operation
- Selectable Output Current Up to 5A
- Parallelable for Increased Output Current, Even **from Different Voltage Sources**
- Wide Input Voltage Range: 6V to 36V
- <sup>n</sup> **1.2V to 24V Output Voltage**
- Selectable Switching Frequency: 100kHz to 1MHz
- SnPb or RoHS Compliant Finish
- **Programmable Soft-Start**
- (11.25mm  $\times$  15mm  $\times$  2.82mm) LGA and (11.25mm  $\times$  15mm  $\times$  3.42mm BGA Packages

# **APPLICATIONS**

- SuperCap Charging
- General Purpose Industrial
- Extreme Short-Circuit Protection or Accurate Output Current Limit
- µController-Based Battery Charging
- High Power LED Drive
- Multiple Input, Single Output Voltage Conversion

# FEATURES DESCRIPTION

The LTM®8026 is a 36V<sub>IN</sub>, 5A constant-voltage, constantcurrent (CVCC) step-down µModule® regulator. Includedin the package are the switching controller, power switches, inductor and support components. Operating over an input voltage range of 6V to 36V, the LTM8026 supports an output voltage range of 1.2V to 24V. CVCC operation allows the LTM8026 to accurately regulate its output current up to 5A over the entire output range. The output current can be set by a control voltage, a single resistor or a thermistor. Only resistors to set the output voltage and frequency and the bulk input and output filter capacitors are needed to finish the design.

36V<sub>IN</sub>, 5A CVCC Step-Down

µModule Regulator

The LTM8026 is packaged in a thermally-enhanced, compact (11.25mm  $\times$  15mm) overmolded land grid array (LGA) and ball grid array (BGA) packages suitable for automated assembly by standard surface mount equipment. The LTM8026 is available in SnPb (BGA) or RoHS compliant terminal finish.

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# TYPICAL APPLICATION



V<sub>OUT</sub> vs I<sub>OUT</sub>, 12V<sub>IN</sub>



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# ABSOLUTE MAXIMUM RATINGS

**(Note 1)**





#### PIN CONFIGURATION **http://www.linear.com/product/LTM8026#orderinfo**



# ORDER INFORMATION



Consult Marketing for parts specified with wider operating temperature ranges. \*Device temperature grade is indicated by a label on the shipping container. Pad or ball finish code is per IPC/JEDEC J-STD-609.

• Terminal Finish Part Marking: www.linear.com/leadfree

• Recommended LGA and BGA PCB Assembly and Manufacturing Procedures:

www.linear.com/umodule/pcbassembly

• LGA and BGA Package and Tray Drawings: www.linear.com/packaging

### **ELECTRICAL CHARACTERISTICS** The  $\bullet$  denotes the specifications which apply over the full internal

operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. RUN = 3V, unless otherwise noted. (Note 3)



**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** This µModule regulator includes overtemperature protection that is intended to protect the device during momentary overload conditions. Internal temperature will exceed 125°C when overtemperature protection is active. Continuous operation above the specified maximum internal operating junction temperature may impair device reliability.

**Note 3:** The LTM8026E is guaranteed to meet performance specifications from 0°C to 125°C internal operating temperature. Specifications over the full –40°C to 125°C internal operating temperature range are assured by design, characterization and correlation with statistical process controls. The LTM8026I is guaranteed to meet specifications over the full –40°C to 125°C internal operating temperature range. The LTM8026MP is guaranteed to meet specifications over the full –55°C to 125°C internal operating temperature range. Note that the maximum internal temperature is determined by specific operating conditions in conjunction with board layout, the rated package thermal resistance and other environmental factors.

**Note 4:** Current flows out of pin.

**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**

8026 G07



8026 G08

8026fd

8026 G09

#### TYPICAL PERFORMANCE CHARACTERISTICS  $T_A = 25^\circ \text{C}$ , unless otherwise noted.

**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**



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**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**







**Input Current vs Output Current 12VOUT**





**Input Current vs Output Current 18VOUT**



**Input Current vs Load Current** 

**–3.3VOUT**

 $1.6$   $\frac{12V_{\text{IN}}}{\sqrt{12V_{\text{IN}}}}$ 

24V<sub>IN</sub> 32.5V<sub>IN</sub>

0

0.6 0.8 1.0

1.2 1.4

0.4 0.2 0

**Input Current vs Output Current 24VOUT**



**Input Current vs Load Current –5VOUT**



8026fd

OUTPUT CURRENT (A)

1 2 4

3 5

8026 G26

**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**



**Minimum Required Input Running Voltage vs Output Voltage,**  8026 G28



**Minimum Required Input Voltage vs Load 8V<sub>OUT</sub>** 







**Minimum Required Input Voltage**   $vs$  Load 3.3V $_{OUT}$  and Below



**Minimum Required Input Voltage** 

**vs Load 12V<sub>OUT</sub>** 

0 13.2

13.4

13.6

13.8

14.0

14.2

14.4

INPUT VOLTAGE (V)

**Minimum Required Input Voltage vs Load 5V<sub>OUT</sub>** 



**Minimum Required Input Voltage vs Load 18V<sub>OUT</sub>** 



LOAD CURRENT (A)

8026 G35

5

1 2 3 4

**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**





**Minimum Required Input Voltage** 



**Minimum Required Input Voltage**  vs Load -8V<sub>OUT</sub>



**Temperature Rise vs Load Current 3.3VOUT**



**Minimum Required Input Voltage**   $vs$  Load  $-12V$ <sub>OUT</sub>



**Temperature Rise vs Load Current**   $5V<sub>OUT</sub>$ 



**Temperature Rise vs Load Current 2.5V<sub>OUT</sub>** 



**Temperature Rise vs Load Current 8V**<sub>OUT</sub>



**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**



8026fd

SWITCHING FREQUENCY (MHz)

0.2 0.4 0.6 1.0

0.8

8026 G53

0

200

100

50  $\pmb{0}$ 

150

8026 G52

LOAD CURRENT (A)

1 2 3 4

0

 $\boldsymbol{0}$ 

40

20

**TA = 25°C, unless otherwise noted. Configured per Table 1, where applicable.**



### PIN FUNCTIONS

V<sub>OUT</sub> (Bank 1): Power Output Pins. Apply the output filter capacitor and the output load between these pins and GND pins.

**GND (Bank 2):** Tie these GND pins to a local ground plane below the LTM8026 and the circuit components. In most applications, the bulk of the heat flow out of the LTM8026 is through these pads, so the printed circuit design has a large impact on the thermal performance of the part. See the PCB Layout and Thermal Considerations sections for more details. Return the feedback divider  $(R_{AD,I})$  to this net.

V<sub>IN</sub> (Bank 3): The V<sub>IN</sub> pins supply current to the LTM8026's internal regulator and to the internal power switches. These pins must be locally bypassed with an external, low ESR capacitor; see Table 1 for recommended values.

**CTL T (Pin D8):** Connect a resistor/NTC thermistor network to the CTL\_T pin to reduce the maximum regulated output current of the LTM8026 in response to temperature. The maximum control voltage is 1.5V. If this function is not used, tie this pin to  $V_{\text{RFF}}$ .

**CTL\_I (Pin E8):** The CTL\_I pin reduces the maximum regulated output current of the LTM8026. The maximum control voltage is 1.5V. If this function is not used, tie this pin to  $V_{\text{RFF}}$ .

**VREF (Pin F8):** Buffered 2V Reference Capable of 0.5mA Drive.

**RT (Pin G8):** The RT pin is used to program the switching frequency of the LTM8026 by connecting a resistor from this pin to ground. The Applications Information section of the data sheet includes a table to determine the resistance value based on the desired switching frequency. When using the SYNC function, apply a resistor value equivalent to 20% lower than the SYNC pulse frequency. Do not leave this pin open.

**COMP (Pin H8):** Compensation Pin. This pin is generally not used. The LTM8026 is internally compensated, but some rare situations may arise that require a modification to the control loop. This pin connects directly to the PWM comparatoroftheLTM8026. Inmost cases, noadjustment is necessary. If this function is not used, leave this pin open.

### PIN FUNCTIONS

**SS (Pin J8):** The Soft-Start Pin. Place an external capacitor to ground to limit the regulated current during start-up conditions. The soft-start pin has an  $11\mu$ A charging current.

**ADJ (Pin K8):**TheLTM8026 regulates itsADJpinto 1.19V. Connect the adjust resistor from this pin to ground. The value of  $R_{ADJ}$  is given by the equation:

$$
R_{ADJ} = \frac{11.9}{V_{OUT} - 1.19}
$$

where  $R_{ADJ}$  is in kΩ.

**RUN (Pin L6):** The RUN pin acts as an enable pin and turns on the internal circuitry. The RUN pin is internally clamped, so it may be pulled up to a voltage source that is higher than the absolute maximum voltage of 6V through a resistor, provided the pin current does not exceed 100µA. Do not leave this pin open. It may also be used to implement a precision UVLO. See the Applications Information section for details.

**SYNC (Pin L7):** Frequency Synchronization Pin. This pin allows the switching frequency to be synchronized to an external clock. The  $R<sub>T</sub>$  resistor should be chosen to operate the internal clock at 20% lower than the SYNC pulse frequency. This pin should be grounded when not in use. Do not leave this pin floating. When laying out the board, avoid noise coupling to or from the SYNC trace. See the Synchronization section in Applications Information.

# BLOCK DIAGRAM



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# **OPERATION**

The LTM8026 is a standalone nonisolated step-down switching DC/DC power supply that can deliver up to 5A of output current. This µModule regulatorprovides a precisely regulated output voltage programmable via one external resistor from 1.2V to 24V. The input voltage range is 6V to 36V. Given that the LTM8026 is a step-down converter, make sure that the input voltage is high enough to support the desired output voltage and load current.

As shown in the Block Diagram, the LTM8026 contains a current mode controller, power switches, power inductor, and a modest amount of input and output capacitance.

The LTM8026 utilizes fixed frequency, average current mode control to accurately regulate the inductor current, independently from the output voltage. This is an ideal solution for applications requiring a regulated current source. The control loop will regulate the current in the internal inductor. Once the output has reached the regulation voltage determined by the resistor from the ADJ pin to ground, the inductor current will be reduced by the voltage regulation loop.

The current control loop has two reference inputs, determined by the voltage at the analog control pins, CTL | and CTL\_T. CTL\_I is typically used to set the maximum allowable current output of the LTM8026, while CTL\_T is typically used with a NTC thermistor to reduce the output current in response to temperature. The lower of the two analog voltages on CTL\_I and CTL\_T determines the regulated output current. The analog control range of both the CTL\_I and CTL\_T pin is from 0V to 1.5V.

The RUN pin functions as a precision shutdown pin. When the voltage at the RUN pin is lower than 1.55V, switching is terminated. Below the turn-on threshold, the RUN pin sinks 5.5µA. This current can be used with a resistor between RUN and  $V_{IN}$  to the set a hysteresis. During startup, the SS pin is held low until the part is enabled, after which the capacitor at the soft-start pin is charged with an 11µA current source.

The LTM8026 is equipped with a thermal shutdown to protect the device during momentary overload conditions. It is set above the 125°C absolute maximum internal temperature rating to avoid interfering with normal specified operation, so internal device temperatures will exceed the absolute maximum rating when the overtemperature protection is active. So, continuous or repeated activation of the thermal shutdown may impair device reliability. During thermal shutdown, all switching is terminated and the SS pin is driven low.

The switching frequency is determined by a resistor at the RT pin. The LTM8026 may also be synchronized to an external clock through the use of the SYNC pin.

For most applications, the design process is straight forward, summarized as follows:

- 1. Look at Table 1 and find the row that has the desired input range and output voltage.
- 2. Apply the recommended  $C_{IN}$ ,  $C_{OUT}$ ,  $R_{ADJ}$  and  $R_{T}$ values.

While these component combinations have been tested for proper operation, it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental conditions. Bear in mind that the maximum output current is limited by junction temperature, the relationship between the input and output voltage magnitude and polarity and other factors. Please refer to the



**Table 1. Recommended Component Values and Configuration. (TA = 25°C. See Typical Performance Characteristics for Load Conditions)**

8026fr

graphs in the Typical Performance Characteristics section for guidance.

The maximum frequency (and attendant  $R_T$  value) at which the LTM8026 should be allowed to switch is given in Table 1 in the  $f_{MAX}$  column, while the recommended frequency (and  $R_T$  value) for optimal efficiency over the given input condition is given in the  $f_{\text{OPTIMAL}}$  column. There are additional conditions that must be satisfied if the synchronization function is used. Please refer to the Switching Frequency Synchronization section for details.

#### **Capacitor Selection Considerations**

The C<sub>IN</sub> and C<sub>OUT</sub> capacitor values in Table 1 are the minimum recommended values for the associated operating conditions. Applying capacitor values below those indicated in Table 1 is not recommended, and may result in undesirable operation. Using larger values is generally acceptable, and can yield improved dynamic response, if necessary. Again, it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental conditions.

Ceramiccapacitorsaresmall, robustandhaveverylowESR. However, not all ceramic capacitors are suitable. X5R and X7R types are stable over temperature, applied voltage and give dependable service. Other types, including Y5V and Z5U have very large temperature and voltage coefficients of capacitance. In an application circuit they may have only a small fraction of their nominal capacitance resulting in much higher output voltage ripple than expected.

Many of the output capacitances given in Table 1 specify an electrolytic capacitor. Ceramic capacitors may also be used in the application, but it may be necessary to use more of them. Many high value ceramic capacitors have a large voltage coefficient, so the actual capacitance of the component at the desired operating voltage may be only a fraction of the specified value. Also, the very low ESR of ceramic capacitors may necessitate additional capacitors for acceptable stability margin.

A final precaution regarding ceramic capacitors concerns the maximum input voltage rating of the LTM8026. A ceramic input capacitor combined with trace or cable inductance forms a high Q (under damped) tank circuit. If the LTM8026 circuit is plugged into a live supply, the input voltage can ring to twice its nominal value, possibly exceeding the device's rating. This situation is easily avoided; see the Hot Plugging Safely section.

#### **Programming Switching Frequency**

The LTM8026 has an operational switching frequency range between 100kHz and 1MHz. This frequency is programmed with an external resistor from the RT pin to ground. Do not leave this pin open under any circumstance. See Table 2 for resistor values and the corresponding switching frequencies.

#### Table 2. R<sub>T</sub> Resistor Values and Their Resultant Switching **Frequencies**



In addition, the Typical Performance Characteristics section contains a graph that shows the switching frequency versus  $R_T$  value.

To improve efficiency at light load, the part will enter discontinuous mode.

#### **Switching Frequency Trade-Offs**

It is recommended that the user apply the optimal  $R<sub>T</sub>$ value given in Table 1 for the input and output operating condition. System level or other considerations, however, may necessitate another operating frequency. While the LTM8026 is flexible enough to accommodate a wide range of operating frequencies, a haphazardly chosen one may result in undesirable operation under certain operating or fault conditions. A frequency that is too high can reduce efficiency, generate excessive heat or even damage the LTM8026 in some fault conditions. A frequency that is too low can result in a final design that has too much output ripple or too large of an output capacitor.

#### **Switching Frequency Synchronization**

8026fd The nominal switching frequency of the LTM8026 is determined by the resistor from the RT pin to GND and

may be set from 100kHz to 1MHz. The internal oscillator may also be synchronized to an external clock through the SYNC pin. The external clock applied to the SYNC pin must have a logic low below 0.6V and a logic high greater than 1.2V. The input frequency must be 20% higher than the frequency determined by the resistor at the RT pin. In general, the duty cycle of the input signal should be greaterthan 10% and less than 90%. Input signals outside ofthese specified parametersmay cause erratic switching behavior and subharmonic oscillations. The SYNC pin must be tied to GND if the synchronization to an external clock is not required. When SYNC is grounded, the switching frequency is determined by the resistor at the RT pin. At light loads, the LTM8026 will enter discontinuous operation to improve efficiency even while a valid clock signal is applied to the SYNC pin.

#### **Soft-Start**

The soft-start function controls the slew rate of the power supply output voltage during start-up. A controlled output voltage ramp minimizes output voltage overshoot, reduces inrush current from the  $V_{IN}$  supply, and facilitates supply sequencing. A capacitor connected from the SS pin to GND programs the slew rate. The capacitor is charged from an internal 11µA current source to produce a ramped output voltage.

#### **Maximum Output Current Adjust**

To adjust the regulated load current, an analog voltage is applied to the CTL\_I pin or CTL\_T pins. Varying the voltage between 0V and 1.5V adjusts the maximum current between the minimum and the maximum current, 5.6A typical. Graphs of the output current vs CTL\_I and CTL\_T voltages are given in the Typical Performance Characteristics section. The LTM8026 provides a 2V reference voltage for conveniently applying resistive dividers to set the current limit. The current limit can be set as shown in Figure 1 with the following equation:

$$
I_{MAX} = \frac{7.467 \cdot R2}{R1 + R2}
$$
 Amps

#### **Load Current Derating Using the CTL\_T Pin**

In high current applications, derating the maximum current based on operating temperature may prevent damage to the load. In addition, many applications have thermal limitations that will require the regulated current to be reduced based on the load and/or board temperature. To achieve this, the LTM8026 uses the CTL\_T pin to reduce the effective regulated current in the load. While CTL\_I programs the regulated current in the load, CTL\_T can be configured to reduce this regulated current based on the analog voltage at the CTL\_T pin. The load/board temperature derating is programmed using a resistor divider with a temperature dependant resistance (Figure 2). When the board/load temperature rises, the CTL\_T voltage will decrease. To reduce the regulated current, the CTL\_T voltage must be lower than the voltage at the CTL\_I pin. CTL\_T may be higher than CTL\_I, but then it will have no effect.

#### **Voltage Regulation and Output Overvoltage Protection**

The LTM8026 uses the ADJ pin to regulate the output voltage and to provide a high speed overvoltage lockout to avoid high voltage conditions. If the output voltage exceeds 125% of the regulated voltage level (1.5V at the ADJ pin), the LTM8026 terminates switching and shuts



Figure 1. Setting the Output Current Limit, I<sub>MAX</sub>





down switching for 13µs. The regulated output voltage must be greater than 1.21V and is set by the equation:

$$
R_{ADJ} = \frac{11.9}{V_{OUT} - 1.19} k\Omega
$$

where  $R_{AD,J}$  is shown in Figure 3.



**Figure 3. Voltage Regulation and Overvoltage Protection Feedback Connections**

### **Thermal Shutdown**

If the part is too hot, the LTM8026 engages its thermal shutdown, terminates switching and discharges the softstart capacitor. When the part has cooled, the part automatically restarts. This thermal shutdown is set to engage at temperatures above the 125°C absolutemaximuminternal operating rating to ensure that it does not interfere with functionality in the specified operating range. This means that internal temperatures will exceed the 125°C absolute maximum rating when the overtemperature protection is active, possibly impairing the device's reliability.

### **Shutdown and UVLO**

TheLTM8026has aninternalUVLOthatterminates switching, resets all logic, and discharges the soft-start capacitor when the input voltage is below 6V. The LTM8026 also has a precision RUN function that enables switching when the voltage at the RUN pin rises to 1.68V and shuts down the LTM8026 when the RUN pin voltage falls to 1.55V. There is also an internal current source that provides 5.5μA of pull-down current to program additional UVLO hysteresis. For RUN rising, the current source is sinking 5.5µA until RUN = 1.68V, after which it turns off. For RUN falling, the current source is off until the RUN = 1.55V, after which it sinks 5.5µA. The following equations determine the voltage

divider resistors for programming the falling UVLO voltage and rising enable voltage ( $V_{ENA}$ ) as configured in Figure 4.

$$
R1 = \frac{1.55 \cdot R2}{UVLO - 1.55}
$$

$$
R2 = \frac{V_{ENA} - 1.084 \cdot UVLO}{5.5 \mu A}
$$

The RUN pin has an absolute maximum voltage of 6V. To accommodate the largest range of applications, there is an internal Zener diode that clamps this pin, so that it can be pulled up to a voltage higher than 6V through a resistor that limits the current to less than 100µA. For applications where the supply range is greater than 4:1, size R2 greater than 375k.



**Figure 4. UVLO Configuration**

#### **Load Sharing**

Two or more LTM8026s may be paralleled to produce higher currents. To do this, simply tie  $V_{\text{OUT}}$ , SS, RUN and ADJ together. The value of the ADJ resistor is given by the equation:

$$
R_{ADJ} = \frac{11.9}{n(V_{OUT} - 1.19)} k\Omega
$$

where n is the number of LTM8026s in parallel. Given the LTM8026's accurate current limit and CVCC operation, each paralleled unit will contribute a portion of the output current, up to the amount determined by the CTL\_I and CTL\_T pins. An example of this is given in the Typical Applications section.

Two or more LTM8026s can share load current equally by using a simple op amp circuit to simultaneously modulate the CTL $\blacksquare$ I pins. Tie SS, RUN, and  $V_{\text{OUT}}$  and CTL $\blacksquare$ I of all of the paralleled LTM8026s together. An example of two

LTM8026s equally sharing output current is shown in the Typical Applications section. The modulation of the CTL\_I inputs is performed at a high bandwidth, so use an op amp with a gain bandwidth product greater than 1MHz. The example circuit in the Typical Applications section uses the LTC6255, which has a minimum gain bandwidth product of 2MHz.

The LTM8026's CVCC operation provides the ability to power share the loadamongseveral input voltage sources. An example of this is shown in the Typical Applications section; please refer to the schematic while reading this discussion. Suppose the application powers 2.5V at 8A and the system under consideration has regulated 24V and 12V input rails available. The power budget for the power rails says that each can allocate only 750mA to produce 2.5V. From the Input Current vs Output Current graph in the Typical Performance Characteristics section for 2.5 $V_{OIII}$ , 750mA from the 24V rail can support more than 5A output current, so apply a  $66.5k/140k$  from  $V_{BFF}$ to the CTL $\perp$ I pin of the LTM8026 powered from 24V<sub>IN</sub> to set the output current to 5A. These resistor values were derived as follows:

- 1. The typical output current limit is 5.6A for CTL\_I = 1.5V and above.
- 2. To get 5A, make the voltage on CTL  $I = 1.5V \cdot 5A/5.6A$  $= 1.34V.$
- 3. The  $V_{\text{RFF}}$  node is a regulated 2V, so applying the 66.5k/140k network yields 2V • 140k/(66.5k + 140k) = 1.35V

The LTM8026 powered from  $12V_{IN}$  needs to supply the rest of the load current, or 3A. Again referring to the Input Current vs Output Current graph in the Typical Performance Characteristics section for  $2.5V<sub>OIII</sub>$ , 750mA will support more than 3A when operated from  $12V_{IN}$ . Using a method similar to the above, apply a resistor network of 132k/78.7k to the CTL\_I pin:

- 1. To get 2.5A, make the voltage on CTL\_I = 1.5V 3A/5.6A  $= 0.8V$
- 2. Applying a 132k/88.7k network to  $V_{\text{RFF}}$  and CTL\_I yields 2V • 88.7k/(88.7k + 132k) = 0.8V



#### **Figure 5. Layout Showing Suggested External Components, GND Plane and Thermal Vias.**

As seen in the graph accompanying the schematic in the Typical Applications section, the input currents to each LTM8026 stays below 750mA for all loads below 8A.

#### **PCB Layout**

Most of the headaches associated with PCB layout have been alleviated or even eliminated by the high level of integration of the LTM8026. The LTM8026 is nevertheless a switching power supply, and care must be taken to minimize EMI and ensure proper operation. Even with the high level of integration, you may fail to achieve specified operation with a haphazard or poor layout. See Figure 5 for a suggested layout. Ensure that the grounding and heat sinking are acceptable.

A few rules to keep in mind are:

- 1. Place the  $R_{AD,J}$  and  $R_T$  resistors as close as possible to their respective pins.
- 2. Place the C<sub>IN</sub> capacitor as close as possible to the V<sub>IN</sub> and GND connection of the LTM8026.

- 3. Place the  $C_{\text{OUT}}$  capacitor as close as possible to the V<sub>OUT</sub> and GND connection of the LTM8026.
- 4. Place the C<sub>IN</sub> and C<sub>OUT</sub> capacitors such that their ground current flow directly adjacent or underneath the LTM8026.
- 5. Connect all of the GND connections to as large a copper pour or plane area as possible on the top layer. Avoid breaking the ground connection between the external components and the LTM8026.
- 6. Use vias to connect the GND copper area to the board's internal ground planes. Liberally distribute these GND vias to provide both a good ground connection and thermal path to the internal planes of the printed circuit board. Pay attention to the location and density of the thermal vias in Figure 5. The LTM8026 can benefit from the heat sinking afforded by vias that connect to internal GND planes at these locations, due to their proximity to internal power handling components. The optimum number of thermal vias depends upon the printed circuit board design. For example, a board might use very small via holes. It should employ more thermal vias than a board that uses larger holes.

### **Hot Plugging Safely**

The small size, robustness and low impedance of ceramic capacitors make them an attractive option for the input bypass capacitor of LTM8026. However, these capacitors can cause problems if the LTM8026 is plugged into a live input supply (see Application Note 88 for a complete discussion). The low loss ceramic capacitor combined with stray inductance in series with the power source forms an underdamped tank circuit, and the voltage at the  $V_{IN}$  pin of the LTM8026 can ring to more than twice the nominal input voltage, possibly exceeding the LTM8026's rating and damaging the part. If the input supply is poorly controlled or the user will be plugging the LTM8026 into an energized supply, the input network should be designed to prevent this overshoot. This can be accomplished by installing a small resistor in series to  $V_{IN}$ , but the most popular method of controlling input voltage overshoot is to add an electrolytic bulk capacitor to the  $V_{IN}$  net. This capacitor's relatively high equivalent series resistance

damps the circuit and eliminates the voltage overshoot. The extra capacitor improves low frequency ripple filtering and can slightly improve the efficiency of the circuit, though it is physically large.

#### **Thermal Considerations**

The LTM8026 output current may need to be derated if it is required to operate in a high ambient temperature. The amount of current derating is dependent upon the input voltage, output power and ambient temperature. The temperature rise curves given in the Typical Performance Characteristics section can be used as a quide. These curves were generated by the LTM8026 mounted to a 58cm<sup>2</sup> 4-layer FR4 printed circuit board. Boards of other sizes and layer count can exhibit different thermal behavior, so it is incumbent upon the user to verify proper operation over the intended system's line, load and environmental operating conditions.

For increased accuracy and fidelity to the actual application, many designers use finite element analysis (FEA) to predict thermal performance. To that end, Page 2 of the data sheet typically gives four thermal coefficients:

 $\theta_{JA}$  – Thermal resistance from junction to ambient

- θJCbottom Thermal resistance from junction to the bottom of the product case
- $\theta_{JCtop}$  Thermal resistance from junction to top of the product case
- $\theta_{\text{JB}}$  Thermal resistance from junction to the printed circuit board.

While the meaning of each of these coefficients may seem to be intuitive, JEDEC has defined each to avoid confusion and inconsistency. These definitions are given in JESD 51-12, and are quoted or paraphrased below:

 $\theta_{JA}$  is the natural convection junction-to-ambient air thermal resistance measured in a one cubic foot sealed enclosure. This environment is sometimes referred to as "still air" although natural convection causes the air to move. This value is determined with the part mounted to a JESD 51-9 defined test board, which does not reflect an actual application or viable operating condition.

 $\theta$ JC hottom is the junction-to-board thermal resistance with all of the component power dissipation flowing through the bottom of the package. In the typical µModule regulator, the bulk of the heat flows out the bottom of the package, but there is always heat flow out into the ambient environment. As a result, this thermal resistance value may be useful for comparing packages but the test conditions don't generally match the user's application.

 $\theta_{JChon}$  is determined with nearly all of the component power dissipation flowing through the top of the package. As the electrical connections of the typical µModule regulator are on the bottom of the package, it is rare for an application to operate such that most of the heat flows from the junction to the top of the part. As in the case of  $\theta_{JCbottom}$ , this value may be useful for comparing packages but the test conditions don't generally match the user's application.

 $\theta_{\text{JB}}$  is the junction-to-board thermal resistance where almost all of the heat flows through the bottom of the µModule regulator and into the board, and is really the sum of the  $\theta_{JCbottom}$  and the thermal resistance of the bottom of the part through the solder joints and through a portion of the board. The board temperature is measured a specified distance from the package, using a 2-sided, 2-layer board. This board is described in JESD 51-9.

Given these definitions, it should now be apparent that none of these thermal coefficients reflects an actual physical operating condition of a µModule regulator. Thus, none of them can be individually used to accurately predict the thermal performance of the product. Likewise, it would be inappropriate to attempt to use any one coefficient to correlate to the junction temperature vs load graphs given in the product's data sheet. The only appropriate way to use the coefficients is when running a detailed thermal analysis, such as FEA, which considers all of the thermal resistances simultaneously.

A graphical representation of these thermal resistances is given in Figure 6.

The blue resistances are contained within the  $µ$ Module device, and the green are outside.

The die temperature of the LTM8026 must be lower than the maximum rating of 125°C, so care should be taken in the layout of the circuit to ensure good heat sinking of the LTM8026. The bulk of the heat flow out of the LTM8026 is through the bottom of the module and the pads into the printed circuit board. Consequently a poor printed circuit board design can cause excessive heating, resulting in impaired performance or reliability. Please refer to the PCB Layout section for printed circuit board design suggestions.





8026fd



**36VIN, 3.3VOUT Step-Down CVCC Converter**











31V<sub>IN</sub>, -5V<sub>OUT</sub> Negative CVCC Converter







Two LTM8026s Operating in Parallel to Produce 2.5V<sub>OUT</sub> at 10A, Equally Sharing Current



**Two LTM8026s Running from 12V and 24V. At Max Load, Each LTM8026 Draws Less Than 750mA from Their Respective Input Sources** 

**Input Current vs Output Current**



# PACKAGE DESCRIPTION



#### **Table 3. Pin Assignment Table (Arranged by Pin Number)**



# PACKAGE PHOTO



### PACKAGE DESCRIPTION

**LGA Package**

LGA Package

**Please refer to http://www.linear.com/product/LTM8026#packaging for the most recent package drawings.**



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### PACKAGE DESCRIPTION

**Please refer to http://www.linear.com/product/LTM8026#packaging for the most recent package drawings.**



# REVISION HISTORY



**36V<sub>IN</sub>, 3.3V<sub>OUT</sub> Step-Down Converter with 4.75A Accurate Current Limit** 



# DESIGN RESOURCES



# RELATED PARTS



