

LT1678

Dual Low Noise, Rail-to-Rail, Precision Op Amps

The LT® 1678/LT1679 are dual/quad rail-to-rail op amps offering both low noise and precision: 3.9nV/√Hz wideband noise, 1/f corner frequency of 4Hz and 90nV peak-to-peak 0.1Hz to 10Hz noise are combined with outstanding precision: 100µV maximum offset voltage, greater than 100dB common mode and power supply rejection and 20MHz gain bandwidth product. The LT1678/LT1679 bring precision as well as low noise to single supply applications as low as 3V. The input range exceeds the power supply by 100mV with no phase inversion while the output can swing

The LT1678/LT1679 are offered in the SO-8 and SO-14 packages. A full set of matching specifications are also provided, facilitating their use in matching dependent applications such as a two op amp instrumentation amplifier design. The LT1678/LT1679 are specified for supply voltages of \pm 15V, single 5V as well as single 3V. For a single amplifier with similiar performance, see the LT1677 data

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DESCRIPTION

to within 170mV of either rail.

sheet.

FEATURES

- **Rail-to-Rail Input and Output**
- **100% Tested Low Voltage Noise: 3.9nV/**√**Hz Typ at 1kHz 5.5nV/**√**Hz Max at 1kHz**
- **Single Supply Operation from 2.7V to 36V**
- **Offset Voltage: 100**µ**V Max**
- Low Input Bias Current: 20nA Max
- High A_{VOL}: $3V/\mu V$ Min, R_L = 10k
- High CMRR: 100dB Min
- High PSRR: 106dB Min
- Gain Bandwidth Product: 20MHz
- Operating Temperature Range: -40° C to 85 $^{\circ}$ C
- Matching Specifications
- No Phase Inversion
- 8-Lead SO and 14-Lead SO Packages

APPLICATIONS

- Strain Gauge Amplifiers
- Portable Microphones
- Battery-Powered Rail-to-Rail Instrumentation
- Low Noise Signal Processing

TYPICAL APPLICATION

- Microvolt Accuracy Threshold Detection
- Infrared Detectors

Instrumentation Amplifier with Shield Driver

0.1Hz to 10Hz Voltage Noise

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ABSOLUTE MAXIMUM RATINGS

(Note 1)

Supply Voltage .. ±18V Input Voltages (Note 2) 0.3V Beyond Either Rail Differential Input Current (Note 2) ± 25mA Output Short-Circuit Duration (Note 3) Indefinite Storage Temperature Range –65°C to 150°C

PACKAGE/ORDER INFORMATION

Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS The \bullet denotes the specifications which apply over the full operating

temperature range, otherwise specifications are at $T_A = 25^\circ \text{C}$. $V_S = 3V$, $V_{CM} = V_0 = 1.7V$; $V_S = 5V$, $V_{CM} = V_0 = 2.5V$ unless **otherwise noted.**

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Note 1: Absolute Maximum Ratings are those values beyond which the life of the device may be impaired.

Note 2: The inputs are protected by back-to-back diodes. Current limiting resistors are not used in order to achieve low noise. If differential input voltage exceeds \pm 1.4V, the input current should be limited to 25mA. If the common mode range exceeds either rail, the input current should be limited to 10mA.

Note 3: A heat sink may be required to keep the junction temperature below absolute maximum.

Note 4: The LT1678C/LT1679C and LT1678I/LT1679I are guaranteed functional over the Operating Temperature Range of –40°C to 85°C.

Note 5: The LT1678C/LT1679C are guaranteed to meet specified performance from 0°C to 70°C. The LT1678C/LT1679C are designed, characterized and expected to meet specified performance from – 40°C to 85°C but is not tested or QA sampled at these temperatures. The LT1678I/ LT1679I are guaranteed to meet specified performance from -40° C to 85°C.

Note 6: Typical parameters are defined as the 60% yield of parameter distributions of individual amplifier; i.e., out of 100 LT1678/LT1679s, typically 60 op amps will be better than the indicated specification.

Note 7: See the test circuit and frequency response curve for 0.1Hz to10Hz tester in the Applications Information section.

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Note 8: Noise is 100% tested at ±15V supplies.
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Note 9: Slew rate is measured in $A_V = -1$; input signal is $\pm 10V$, output measured at \pm 5V.

Note 10: This parameter is not 100% tested.

Note 11: $V_S = 5V$ limits are guaranteed by correlation to $V_S = 3V$ and $V_S = \pm 15V$ tests.

Note 12: $V_S = 3V$ limits are guaranteed by correlation to $V_S = 5V$ and $V_S = \pm 15V$ tests.

Note 13: Guaranteed by correlation to slew rate at $V_S = \pm 15V$ and GBW at $V_S = 3V$ and $V_S = \pm 15V$ tests.

Note 14: ∆CMRR and ∆PSRR are defined as follows:

- 1. CMRR and PSRR are measured in μ V/V on the individual amplifiers.
- 2. The difference is calculated between the matching sides in μ V/V.
- 3. The result is converted to dB.

Note 15: Matching parameters are the difference between amplifiers A and B on the LT1678 and between amplifiers A and D and B and C in the LT1679.

Note 16: Input range guaranteed by the common mode rejection ratio test.

TYPICAL PERFORMANCE CHARACTERISTICS

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APPLICATIONS INFORMATION

Rail-to-Rail Operation

To take full advantage of an input range that can exceed the supply, the LT1678/LT1679 are designed to eliminate phase reversal. Referring to the photographs shown in Figure 1, the LT1678/LT1679 are operating in the follower mode $(A_V = +1)$ at a single 3V supply. The output of the LT1678/LT1679 clips cleanly and recovers with no phase reversal. This has the benefit of preventing lock-up in servo systems and minimizing distortion components.

Figure 1. Voltage Follower with Input Exceeding the Supply Voltage $(V_S = 3V)$

Unity-Gain Buffer Application

When R_F \leq 100 Ω and the input is driven with a fast, largesignal pulse (>1V), the output waveform will look as shown in the pulsed operation diagram (Figure 2).

During the fast feedthrough-like portion of the output, the input protection diodes effectively short the output to the

input and a current, limited only by the output short-circuit protection, will be drawn by the signal generator. With $R_F \geq 500\Omega$, the output is capable of handling the current requirements ($I_1 \le 20$ mA at 10V) and the amplifier stays in its active mode and a smooth transition will occur.

As with all operational amplifiers when $R_F > 2k$, a pole will be created with R_F and the amplifier's input capacitance, creating additional phase shift and reducing the phase margin. A small capacitor (20pF to 50pF) in parallel with R_F will eliminate this problem.

Figure 2. Pulsed Operation

Noise Testing

The 0.1Hz to 10Hz peak-to-peak noise of the LT1678/ LT1679 are measured in the test circuit shown (Figure 3). The frequency response of this noise tester (Figure 4) indicates that the 0.1Hz corner is defined by only one zero. The test time to measure 0.1Hz to 10Hz noise should not exceed ten seconds, as this time limit acts as an additional zero to eliminate noise contributions from the frequency band below 0.1Hz.

Measuring the typical 90nV peak-to-peak noise performance of the LT1678/LT1679 requires special test precautions:

- 1. The device should be warmed up for at least five minutes. As the op amp warms up, its offset voltage changes typically 3µV due to its chip temperature increasing 10°C to 20°C from the moment the power supplies are turned on. In the ten-second measurement interval these temperature-induced effects can easily exceed tens of nanovolts.
- 2. For similar reasons, the device must be well shielded from air currents to eliminate the possibility of thermoelectric effects in excess of a few nanovolts, which would invalidate the measurements.

APPLICATIONS INFORMATION

Figure 3. 0.1Hz to 10Hz Noise Test Circuit

3. Sudden motion in the vicinity of the device can also "feedthrough" to increase the observed noise.

Current noise is measured in the circuit shown in Figure 5 and calculated by the following formula:

Figure 5.

The LT1678/LT1679 achieve their low noise, in part, by operating the input stage at 100µA versus the typical 10µA of most other op amps. Voltage noise is inversely proportional while current noise is directly proportional to the square root of the input stage current. Therefore, the LT1678/LT1679's current noise will be relatively high. At low frequencies, the low 1/f current noise corner frequency (≈200Hz) minimizes current noise to some extent.

In most practical applications, however, current noise will not limit system performance. This is illustrated in the Total Noise vs Source Resistance plot (Figure 6) where:

Figure 4. 0.1Hz to 10Hz Peak-to-Peak Noise Tester Frequency Response

Total Noise = $[(op \, amp \, voltage \, noise)^2 + (resistor \, noise)^2]$ + (current noise R_S)²]^{1/2}

Three regions can be identified as a function of source resistance:

- (i) $R_S \le 400\Omega$. Voltage noise dominates
- (ii) 400Ω ≤ R_S ≤ 50k at 1kHz 400Ω ≤ R_S ≤ 8k at 10Hz Resistor Noise Dominates
- (iii) R_S > 50k at 1kHz R_S > 8k at 10Hz Current Noise Dominates

Clearly the LT1678/LT1679 should not be used in region (iii), where total system noise is at least six times higher than the voltage noise of the op amp, i.e., the low voltage noise specification is completely wasted. In this region the LT1113 or LT1169 are better choices.

APPLICATIONS INFORMATION

Rail-to-Rail Input

The input common mode range for the LT1678/LT1679 can exceed the supplies by at least 100mV. As the common mode voltage approaches the positive rail $(+V_S)$ – 0.7V), the tail current for the input pair (Q1, Q2) is reduced, which prevents the input pair from saturating (refer to the Simplified Schematic). The voltage drop across the load resistors R_{C1} , R_{C2} is reduced to less than 200mV, degrading the slew rate, bandwidth, voltage noise, offset voltage and input bias current (the cancellation is shut off).

When the input common mode range goes below 1.5V above the negative rail, the NPN input pair (Q1, Q2) shuts off and the PNP input pair (Q8, Q9) turns on. The offset voltage, input bias current, voltage noise and bandwidth are also degraded. The graph of Offset Voltage Shift vs Common Mode shows where the knees occur by displaying the change in offset voltage. The change-over points are temperature dependent; see the graph Common Mode Range vs Temperature.

Rail-to-Rail Output

The rail-to-rail output swing is achieved by using transistor collectors (Q28, Q29 referring to the Simplified Schematic) instead of customary class A-B emitter followers for the output stage. The output NPN transistor (Q29) sinks the current necessary to move the output in the negative direction. The change in Q29's base emitter voltage is reflected directly to the gain node (collectors of Q20 and Q16). For large sinking currents, the delta V_{BF} of Q29 can dominate the gain. Figure 7 shows the change in input voltage for a change in output voltage for different load resistors connected between the supplies. The gain is much higher for output voltages above ground (Q28 sources current) since the change in base emitter voltage of Q28 is attenuated by the gain in the PNP portion of the output stage. Therefore, for positive output swings (output sourcing current) there is hardly any change in input voltage for any load resistance. Highest gain and best linearity are achieved when the output is sourcing current, which is the case in single supply operation when the load is ground referenced. Figure 8 shows gains for both sinking and sourcing load currents for a worst-case load of 600Ω.

Figure 7. Voltage Gain Split Supply Figure 8. Voltage Gain Single Supply

SIMPLIFIED SCHEMATIC

U PACKAGE DESCRIPTIO

S8 Package 8-Lead Plastic Small Outline (Narrow .150 Inch) (Reference LTC DWG # 05-08-1610)

S Package 14-Lead Plastic Small Outline (Narrow .150 Inch) (Reference LTC DWG # 05-08-1610)

.337 – .344 $.045 \pm .005$ $(8.560 - 8.738)$.050 BSC NOTE 3 $\frac{1}{\sqrt{2}}$ 8 14 13 12 11 10 9 N F Ħ F N 245 $.160 \pm .005$ MIN .150 – .157 $.228 - .244$ $(\overline{5.791} - 6.197)$ (3.810 – 3.988) NOTE 3 1 2 3 N/2 N/2 $.030 \pm .005$ 5 6 7 $\begin{array}{ccc} \square & \square & \square \\ \square & \square & \square \\ \square & \square & \square \end{array}$ TYP $\frac{1}{1}$ 目 RECOMMENDED SOLDER PAD LAYOUT $.010 - .020$ $\frac{.010 - .020}{(0.254 - 0.508)}$ × 45° $.053 - .069$ $(\overline{1.346 - 1.752})$.004 – .010 $.008 - .010$ $(0.101 - 0.254)$ $(0.203 - 0.254)$ $0^\circ - 8^\circ$ TYP $.014 - .019$.050 $.016 - .050$ $(0.355 - 0.483)$ (1.270) $(0.406 - 1.270)$ TYP BSC NOTE: S14 0502 INCHES 1. DIMENSIONS IN **MILLIMETERS** 2. DRAWING NOT TO SCALE

3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

Information furnished by Linear Technology Corporation is believed to be accurate and reliable. However, no responsibility is assumed for its use. Linear Technology Corporation makes no representation that the interconnection of its circuits as described herein will not infringe on existing patent rights.

TYPICAL APPLICATIO U

Bridge Reversal Eliminates 1/f Noise and Offset Drift of a Low Noise, Non-autozeroed, Bipolar Amplifier. Circuit Gives 14nV Noise Level or 19 Effective Bits Over a 10mV Span

RELATED PARTS

