

Data Sheet **AD8051**

FEATURES

High speed and fast settling on 5 V 110 MHz, −3 dB bandwidth (G = +1) (AD8051/AD8052) 150 MHz, −3 dB bandwidth (G = +1) (AD8054) 145 V/μs slew rate 50 ns settling time to 0.1% Single-supply operation Output swings to within 25 mV of either rail Input voltage range: −0.2 V to +4 V; Vs = 5 V Video specifications (G = +2) 0.1 dB gain flatness: 20 MHz; RL = 150 Ω Differential gain/phase: 0.03%/0.03° Low distortion −80 dBc total harmonic @ 1 MHz, RL = 100 Ω Outstanding load drive capability Drives 45 mA, 0.5 V from supply rails (AD8051/AD8052) Drives 50 pF capacitive load (G = +1) (AD8051/AD8052) Low power: 2.75 mA/amplifier (AD8054) Low power: 4.4 mA/amplifier (AD8051/AD8052)

APPLICATIONS

Active filters Analog-to-digital drivers Clock buffer Consumer video Professional cameras CCD imaging systems CD/DVD ROMs

PIN CONNECTIONS (TOP VIEWS)

Low Cost, High Speed,

Rail-to-Rail Amplifiers

Figure 3. SOIC (R-8) and MSOP (RM-8) Figure 4. SOIC (R-14) and TSSOP (RU-14)

GENERAL DESCRIPTION

The AD8051 (single), AD8052 (dual), and AD8054 (quad) are low cost, high speed, voltage feedback amplifiers. The amplifiers operate on $+3$ V, $+5$ V, or ± 5 V supplies at low supply current. They have true single-supply capability with an input voltage range extending 200 mV below the negative rail and within 1 V of the positive rail.

Despite their low cost, the AD8051/AD8052/AD8054 provide excellent overall performance and versatility. The output voltage swings to within 25 mV of each rail, providing maximum output dynamic range with excellent overdrive recovery.

Rev. K Document Feedback

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The AD8051/AD8052/AD8054 are well suited for video electronics, cameras, video switchers, or any high speed portable equipment. Low distortion and fast settling make them ideal for active filter applications.

The AD8051/AD8052 in the 8-lead SOIC, the AD8052 in the MSOP, the AD8054 in the 14-lead SOIC, and the 14-lead TSSOP packages are available in the extended temperature range of −40°C to +125°C.

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REVISION HISTORY

12/2008—Rev. H to Rev. I

12/2007—Rev. G to Rev. H

5/2006—Rev. F to Rev. G

2/2003—Rev. C to Rev. D

SPECIFICATIONS

@ T_A = 25°C, V_S = 5 V, R_L = 2 k Ω to 2.5 V, unless otherwise noted.

Table 1.

1 Refer t[o Figure 19.](#page-11-0)

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@ T_A = 25°C, V_S = 3 V, R_L = 2 kΩ to 1.5 V, unless otherwise noted.

Table 2.

1 Refer t[o Figure 19.](#page-11-0)

@ T_A = 25°C, V_S = ±5 V, R_L = 2 kΩ to ground, unless otherwise noted.

Table 3.

ABSOLUTE MAXIMUM RATINGS

Table 4.

1 Se[e Table 5.](#page-8-4)

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

THERMAL RESISTANCE

Specification is for device in free air.

MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD8051/AD8052/AD8054 is limited by the associated rise in junction temperature. The maximum safe junction temperature for plastic encapsulated devices is determined by the glass transition temperature of the plastic, approximately 150°C. Temporarily exceeding this limit can cause a shift in parametric performance due to a change in the stresses exerted on the die by the package. Exceeding a junction temperature of 175°C for an extended period can result in device failure.

While the AD8051/AD8052/AD8054 are internally shortcircuit protected, this cannot be sufficient to guarantee that the maximum junction temperature (150°C) is not exceeded under all conditions. To ensure proper operation, it is necessary to observe the maximum power derating curves.

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

TYPICAL PERFORMANCE CHARACTERISTICS

Figure 7. AD8051/AD8052 Normalized Gain vs. Frequency; $V_S = 5$ V

Figure 9. AD8051/AD8052 Gain vs. Frequency vs. Temperature

Figure 10. AD8054 Normalized Gain vs. Frequency; $V_S = 5$ V

Figure 12. AD8054 Gain vs. Frequency vs. Temperature

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Figure 13. AD8051/AD8052 0.1 dB Gain Flatness vs. Frequency; $G = +2$

Figure 15. AD8051/AD8052 Open-Loop Gain and Phase vs. Frequency

Figure 16. AD8054 0.1 dB Gain Flatness vs. Frequency; $G = +2$

Figure 18. AD8054 Open-Loop Gain and Phase Margin vs. Frequency

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RL = 150Ω

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RL = 150Ω

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RL = 1kΩ

–10 $V_S = 5V$ **–20 RF = 2kΩ RL = 2kΩ –30 VOUT = 2V p-p –40** CROSSTALK (dB) **CROSSTALK (dB) –50 –60 –70 –80** \mathbf{H} **–90 –100** 062-025 01062-025 **FREQUENCY (MHz) 0.1 500 100 1 10**

Figure 25. AD8052 Crosstalk (Output-to-Output) vs. Frequency

Figure 27. Closed-Loop Output Resistance vs. Frequency

Figure 28. AD8054 Crosstalk (Output-to-Output) vs. Frequency

Figure 31. AD8051/AD8052 Output Saturation Voltage vs. Load Current

Figure 33. AD8054 Output Saturation Voltage vs. Load Current

Figure 32. Open-Loop Gain vs. Output Voltage

Figure 34. 100 mV Step Response, $G = +1$

Figure 35. AD8051/AD8052 200 mV Step Response; $V_S = 5 V$, $G = +1$

Figure 37. Output Swing; $G = -1$, $R_L = 2 k\Omega$

Figure 38. AD8054 100 mV Step Response; $V_S = 5 V$, $G = +1$

Figure 39. Large Signal Step Response; $V_s = \pm 5$ V, $G = +1$

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THEORY OF OPERATION **CIRCUIT DESCRIPTION**

The AD8051/AD8052/AD8054 are fabricated on the Analog Devices, Inc. proprietary eXtra-Fast Complementary Bipolar (XFCB) process, which enables the construction of PNP and NPN transistors with similar fTs in the 2 GHz to 4 GHz region. The process is dielectrically isolated to eliminate the parasitic and latch-up problems caused by junction isolation. These features allow the construction of high frequency, low distortion amplifiers with low supply currents. This design uses a differential output input stage to maximize bandwidth and headroom (see [Figure 40\)](#page-15-2). The smaller signal swings required on the first stage outputs (nodes SIP, SIN) reduce the effect of nonlinear currents due to junction capacitances and improve the distortion performance. This design achieves harmonic distortion of −80 dBc ω 1 MHz into 100 Ω with V_{OUT} = 2 V p-p (gain = +1) on a single 5 V supply.

The inputs of the device can handle voltages from −0.2 V below the negative rail to within 1 V of the positive rail. Exceeding these values do not cause phase reversal; however, the input ESD devices begin to conduct if the input voltages exceed the rails by greater than 0.5 V. During this overdrive condition, the output stays at the rail.

The rail-to-rail output range of the AD8051/AD8052/AD8054 is provided by a complementary common emitter output stage. High output drive capability is provided by injecting all output stage predriver currents directly into the bases of the output devices Q8 and Q36. Biasing of Q8 and Q36 is accomplished by I8 and I5, along with a common-mode feedback loop (not shown). This circuit topology allows the AD8051/AD8052 to drive 45 mA of output current and allows the AD8054 to drive 30 mA of output current with the outputs within 0.5 V of the supply rails.

Figure 40. AD8051/AD8052 Simplified Schematic

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APPLICATIONS INFORMATION **OVERDRIVE RECOVERY**

Overdrive of an amplifier occurs when the output and/or input range is exceeded. The amplifier must recover from this overdrive condition. As shown i[n Figure 41,](#page-16-3) the AD8051/AD8052/ AD8054 recover within 60 ns from negative overdrive and within 45 ns from positive overdrive.

DRIVING CAPACITIVE LOADS

Consider the AD8051/AD8052 in a closed-loop gain of +1 with $+V_s = 5$ V and a load of 2 kΩ in parallel with 50 pF. Figure 42 an[d Figure 43](#page-16-5) show their frequency and time domain responses, respectively, to a small-signal excitation. The capacitive load drive of the AD8051/AD8052/AD8054 can be increased by adding a low value resistor in series with the load. [Figure 44](#page-16-6) an[d Figure 45](#page-16-7) show the effect of a series resistor on the capacitive drive for varying voltage gains. As the closed-loop gain is increased, the larger phase margin allows for larger capacitive loads with less peaking. Adding a series resistor with lower closed-loop gains accomplishes the same effect. For large capacitive loads, the frequency response of the amplifier is dominated by the roll-off of the series resistor and the load capacitance.

Figure 42. AD8051/AD8052 Closed-Loop Frequency Response; $C_L = 50$ pF

Figure 43. AD8051/AD8052 200 mV Step Response; $C_l = 50$ pF

Figure 44. AD8051/AD8052 Capacitive Load Drive vs. Closed-Loop Gain

Figure 45. AD8054 Capacitive Load Drive vs. Closed-Loop Gain

LAYOUT CONSIDERATIONS

The specified high speed performance of the AD8051/AD8052/ AD8054 requires careful attention to board layout and component selection. Proper RF design techniques and low parasitic component selection are necessary.

The PCB should have a ground plane covering all unused portions of the component side of the board to provide a low impedance path. The ground plane should be removed from the area near the input pins to reduce parasitic capacitance.

Chip capacitors should be used for supply bypassing. One end should be connected to the ground plane and the other within 3 mm of each power pin. An additional large (4.7 μ F to 10 μ F) tantalum electrolytic capacitor should be connected in parallel, but not necessarily so close, to supply current for fast, large signal changes at the output.

The feedback resistor should be located close to the inverting input pin to keep the parasitic capacitance at this node to a minimum. Parasitic capacitance of less than 1 pF at the inverting input can significantly affect high speed performance.

Stripline design techniques should be used for long signal traces (greater than about 25 mm). These should be designed with a characteristic impedance of 50 Ω or 75 Ω and be properly terminated at each end.

ACTIVE FILTERS

Active filters at higher frequencies require wider bandwidth op amps to work effectively. Excessive phase shift produced by lower frequency op amps can significantly affect active filter performance.

[Figure 46 s](#page-17-2)hows an example of a 2 MHz biquad bandwidth filter that uses three op amps of an AD8054. Such circuits are sometimes used in medical ultrasound systems to lower the

noise bandwidth of the analog signal before analog-to-digital conversion.

Note that the unused amplifier's inputs should be tied to ground.

Figure 46. 2 MHz Biquad Band-Pass Filter Using AD8054

The frequency response of the circuit is shown i[n Figure 47.](#page-17-3)

Figure 47. Frequency Response of 2 MHz Band-Pass Biquad Filter

ANALOG-TO-DIGITAL AND DIGITAL-TO-ANALOG APPLICATIONS

[Figure 50 i](#page-18-1)s a schematic showing the AD8051 used as a driver for an AD9201, a 10-bit, 20 MSPS, dual analog-to-digital converter. This converter is designed to convert I and Q signals in communications systems. In this application, only the I channel is being driven. The I channel is enabled by applying a logic high to SELECT (Pin 13).

The AD8051 is running from a dual supply and is configured for a gain of +2. The input signal is terminated in 50 Ω and the output is 2 V p-p, which is the maximum input range of the AD9201. The 22 Ω series resistor limits the maximum current that flows and helps to lower the distortion of the ADC.

The AD9201 has differential inputs for each channel. These are designated the A and B inputs. The B inputs of each channel are connected to VREF (Pin 22), which supplies a positive reference of 2.5 V. Each of the B inputs has a small low-pass filter that also helps to reduce distortion.

The output of the op amp is ac-coupled into INA-I (Pin 16) via two parallel capacitors to provide good high frequency and low frequency coupling. The 1 k Ω resistor references the signal to VREF that is applied to INB-I. Thus, INA-I swings both positive and negative with respect to the bias voltage applied to INB-I.

With the sampling clock running at 20 MSPS, the analog-todigital output was analyzed with a digital analyzer. Two input frequencies were used, 1 MHz and 9.5 MHz, which is just short of the Nyquist frequency. These signals were well filtered to minimize any harmonics.

[Figure 48 s](#page-18-2)hows the FFT response of the ADC for the case of a 1 MHz analog input. The SFDR is 71.66 dB, and the analog-todigital is producing 8.8 ENOB (effective number of bits). When the analog frequency was raised to 9.5 MHz, the SFDR was

reduced to −60.18 dB and the ADC operated with 8.46 ENOBs as shown i[n Figure 49.](#page-18-3) The inclusion of the AD8051 in the circuit did not worsen the distortion performance of the AD9201.

Fiaure 48. FFT Plot for AD8051 Driving the AD9201 at 1 MHz

Figure 49. FFT Plot for AD8051 Driving the AD9201 at 9.5 MHz

Figure 50. The AD8051 Driving an AD9201, a 10-Bit, 20 MSPS Analog-to-Digital Converter

SYNC STRIPPER

Synchronizing pulses are sometimes carried on video signals so as not to require a separate channel to carry the synchronizing information. However, for some functions, such as analog-todigital conversion, it is not desirable to have the sync pulses on the video signal. These pulses reduce the dynamic range of the video signal and do not provide any useful information for such a function.

A sync stripper removes the synchronizing pulses from a video signal while passing all the useful video information[. Figure 51](#page-19-2) shows a practical single-supply circuit that uses only a single AD8051. It is capable of directly driving a reverse terminated video line.

The video signal plus sync is applied to the noninverting input with the proper termination. The amplifier gain is set to 2 via the two 1 kΩ resistors in the feedback circuit. A bias voltage must be applied to R1 so that the input signal has the sync pulses stripped at the proper level.

The blanking level of the input video pulse is the desired place to remove the sync information. This level is multiplied by 2 by the amplifier. This level must be at ground at the output for the sync stripping action to take place. Since the gain of the amplifier from the input of R1 to the output is -1, a voltage equal to $2 \times V_{BLANK}$ must be applied to make the blanking level come out at ground.

SINGLE-SUPPLY COMPOSITE VIDEO LINE DRIVER

Many composite video signals have their blanking level at ground and have video information that is both positive and negative. Such signals require dual-supply amplifiers to pass them. However, by ac level shifting, a single-supply amplifier can be used to pass these signals. The following complications can arise from such techniques.

Signals of bounded peak-to-peak amplitude that vary in duty cycle require larger dynamic swing capacity than their (bounded) peak-to-peak amplitude after they are ac-coupled. As a worst case, the dynamic signal swing will approach twice the peak-topeak value. The two conditions that define the maximum

dynamic swing requirements are a signal that is mostly low but goes high with a duty cycle that is a small fraction of a percent, and the other extreme defined by the opposite condition.

The worst case of composite video is not quite this demanding. One bounding condition is a signal that is mostly black for an entire frame but has a white (full amplitude) minimum width spike at least once in a frame.

The other extreme is for a full white video signal. The blanking intervals and sync tips of such a signal have negative-going excursions in compliance with the composite video specifications. The combination of horizontal and vertical blanking intervals limit such a signal to being at the highest (white) level for a maximum of about 75% of the time.

As a result of the duty cycles between the two extremes previously presented, a 1 V p-p composite video signal that is multiplied by a gain of 2 requires about 3.2 V p-p of dynamic voltage swing at the output for an op amp to pass a composite video signal of arbitrarily varying duty cycle without distortion.

Some circuits use a sync tip clamp to hold the sync tips at a relatively constant level to lower the amount of dynamic signal swing required. However, these circuits can have artifacts, such as sync tip compression, unless they are driven by a source with a very low output impedance. The AD8051/AD8052/AD8054 have adequate signal swing when running on a single 5 V supply to handle an ac-coupled composite video signal.

The input to the circuit in [Figure 52 i](#page-19-3)s a standard composite (1 V p-p) video signal that has the blanking level at ground. The input network level shifts the video signal by means of ac coupling. The noninverting input of the op amp is biased to half of the supply voltage.

The feedback circuit provides unity gain for the dc-biasing of the input and provides a gain of 2 for any signals that are in the video bandwidth. The output is ac-coupled and terminated to drive the line.

The capacitor values were selected for providing minimum tilt or field time distortion of the video signal. These values would be required for video that is considered to be studio or broadcast quality. However, if a lower consumer grade of video, sometimes referred to as consumer video, is all that is desired, the values and the cost of the capacitors can be reduced by as much as a factor of five with minimum visible degradation in the picture.

Figure 52. Single-Supply Composite Video Line Driver

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OUTLINE DIMENSIONS

ORDERING GUIDE

 $1 Z =$ RoHS Compliant Part. # denotes lead-free product may be top or bottom marked.

NOTES

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